

**WCX**  
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Detroit, Michigan, USA

## **Achieving EM Conducted Emission compliance for high voltage conversion with switching frequency above 1.3 MHz**

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**VICOR**

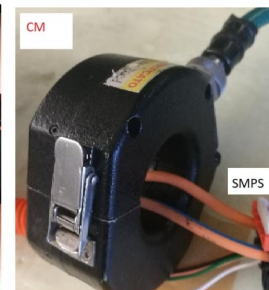
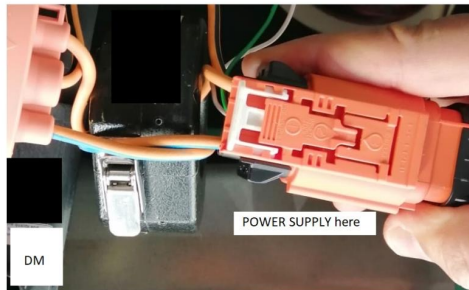
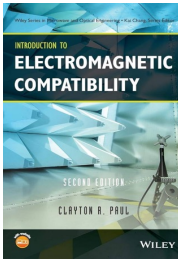
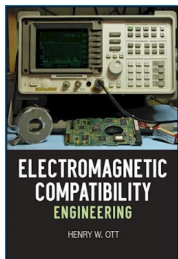
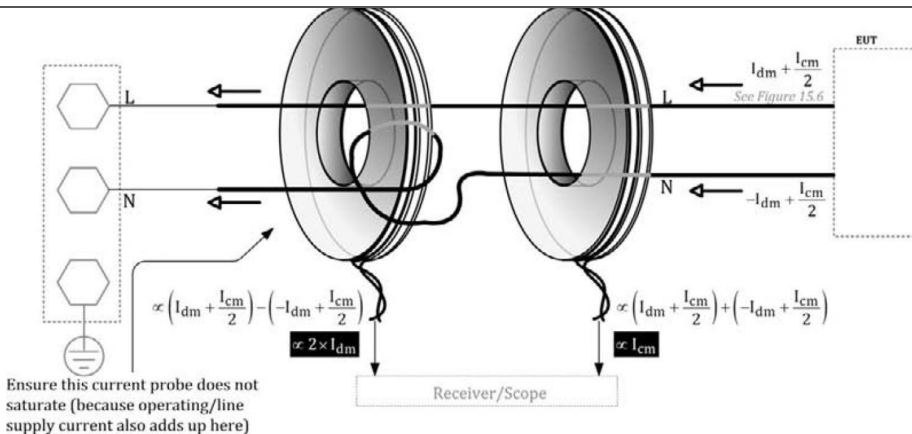
# Agenda

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- Minimum requirements
- The problem
- High frequency noise implications and drawbacks
- Traditional methods and tradeoffs
- The device under test
- EMI baseline
- A potential filter solution
- Conclusions

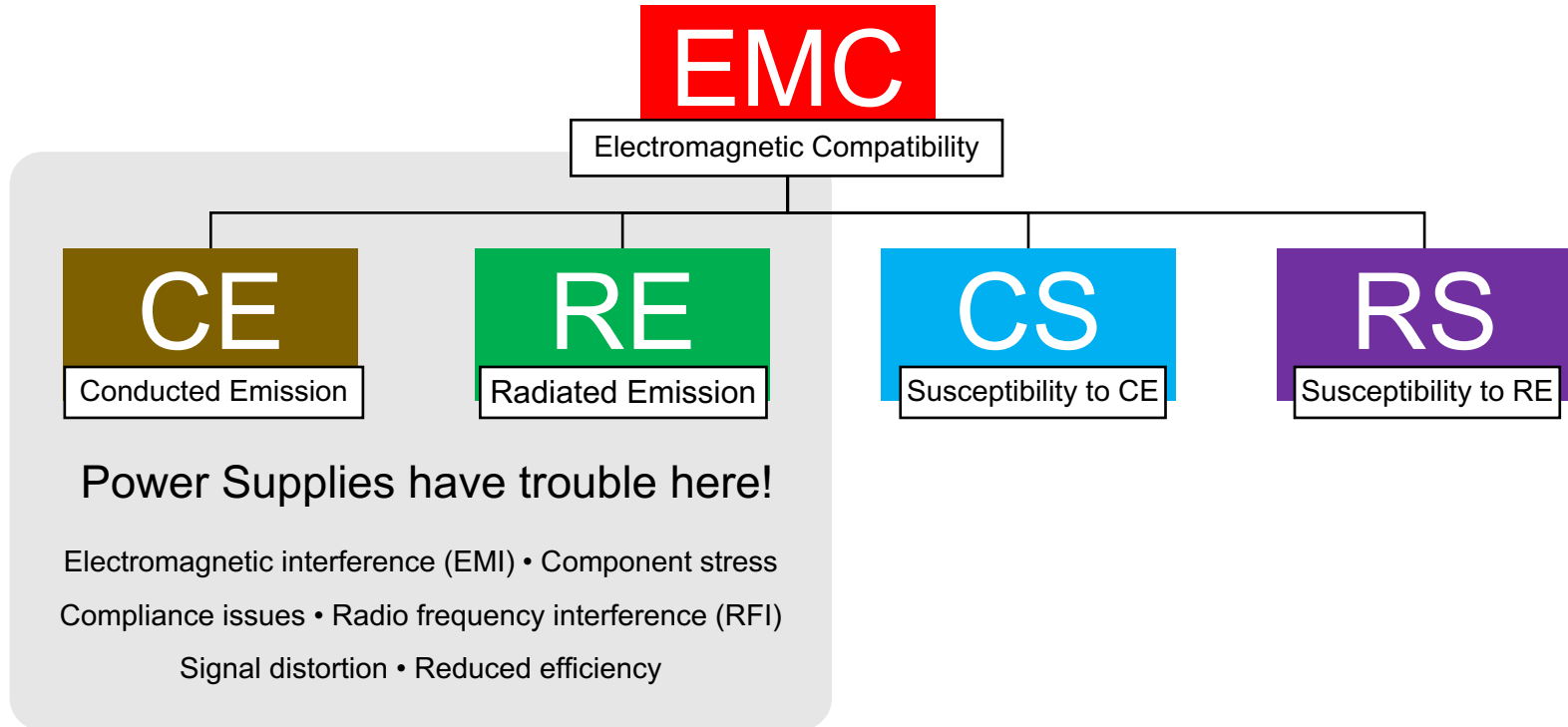
# Background

- Electromagnetic compatibility basics
- Differential Mode (DM) and Common Mode (CM) noise in switching power supplies
- The LISN
- Practical EMI Filter Design course



# High frequency noise implications and drawbacks

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# Traditional methods and tradeoffs

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- Input / output filters
- Shielding
- Grounding techniques
- Snubber circuits
- Spread spectrum techniques
- Soft switching

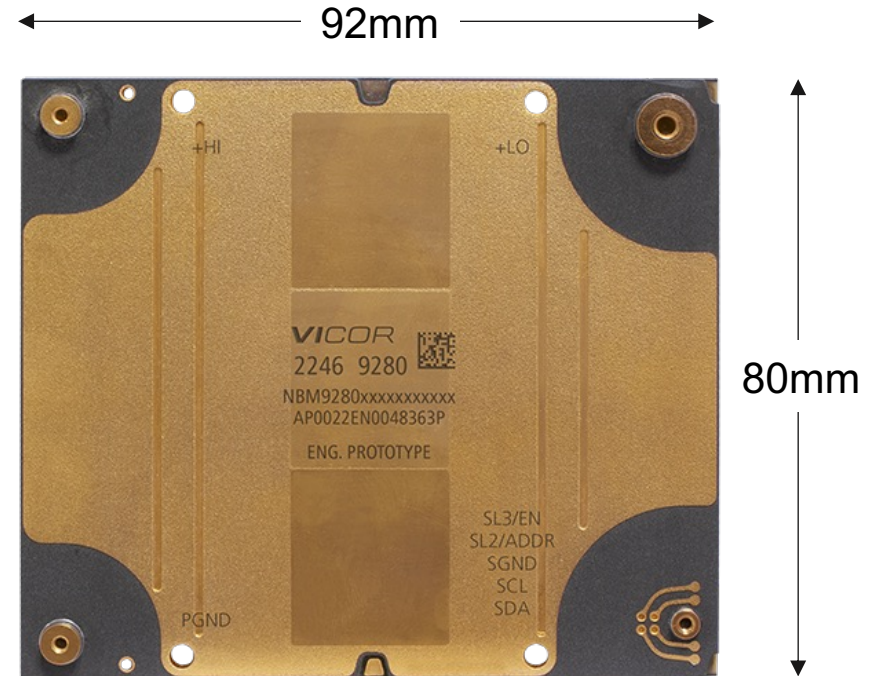


How do we minimize EMI?

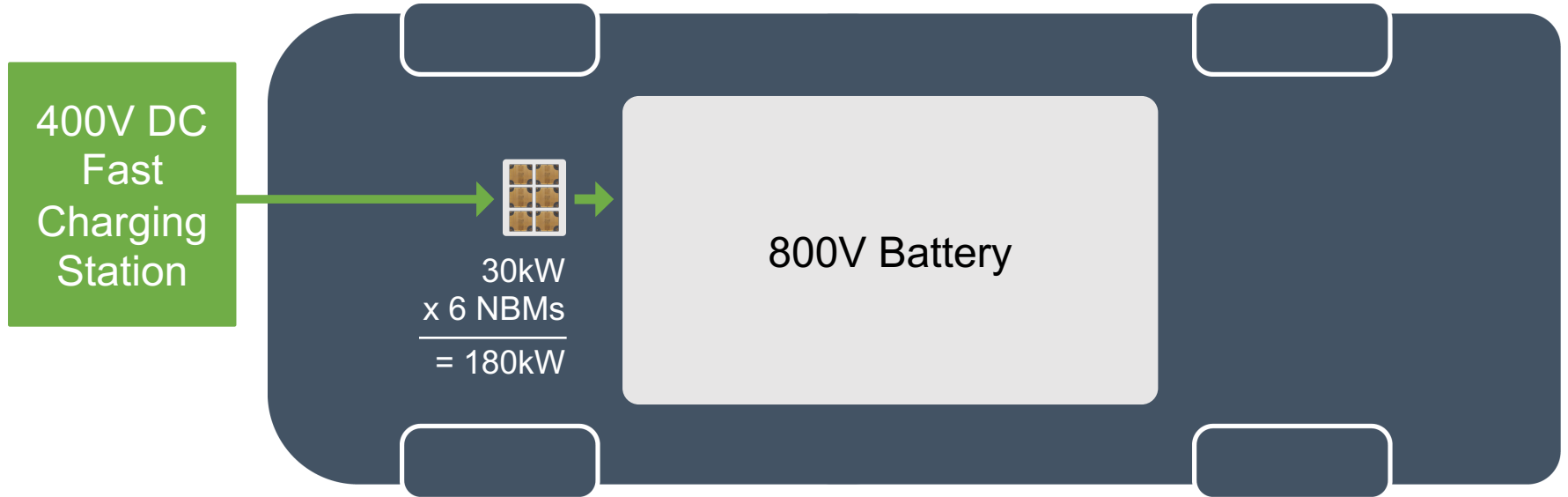
# The Device Under Test (DUT): Vicor NBM9280 power module

- 99% peak efficiency
- Non-isolated
- Bidirectional power flow
- **30kW**

Product Ratings			
Step-Up Operation K = 2/1	$V_{LO} = 400V$ (200 – 460V)	$V_{HI} = 800V$ (400 – 920V) No Load	$I_{HI} = \text{up to } 37.5A$
Step-Down Operation K = 1/2	$V_{HI} = 800V$ (400 – 920V)	$V_{LO} = 800V$ (400 – 920V) No Load	$I_{LO} = \text{up to } 75A$

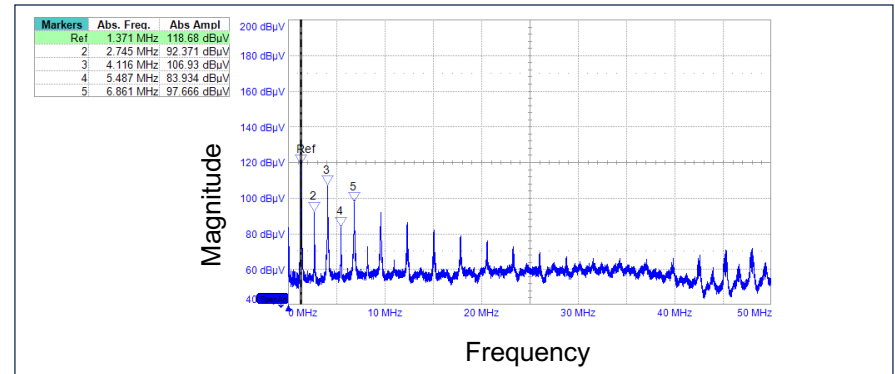
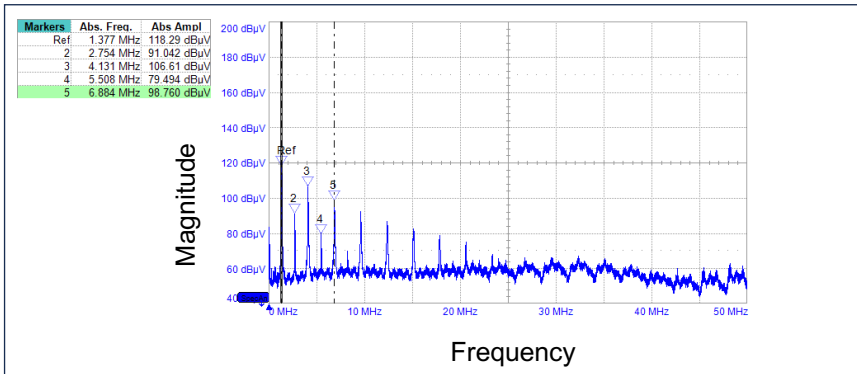
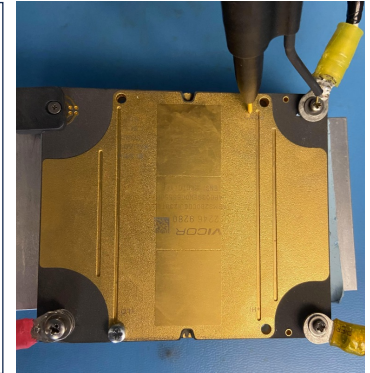
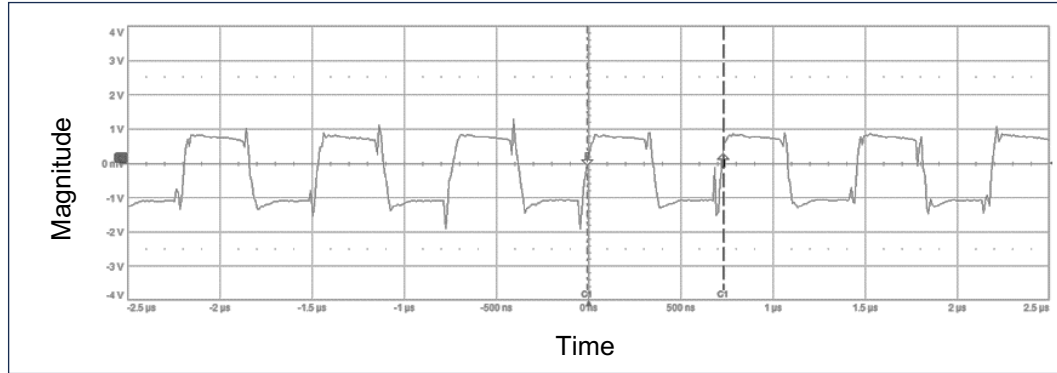


# An automotive application of the NBM9280



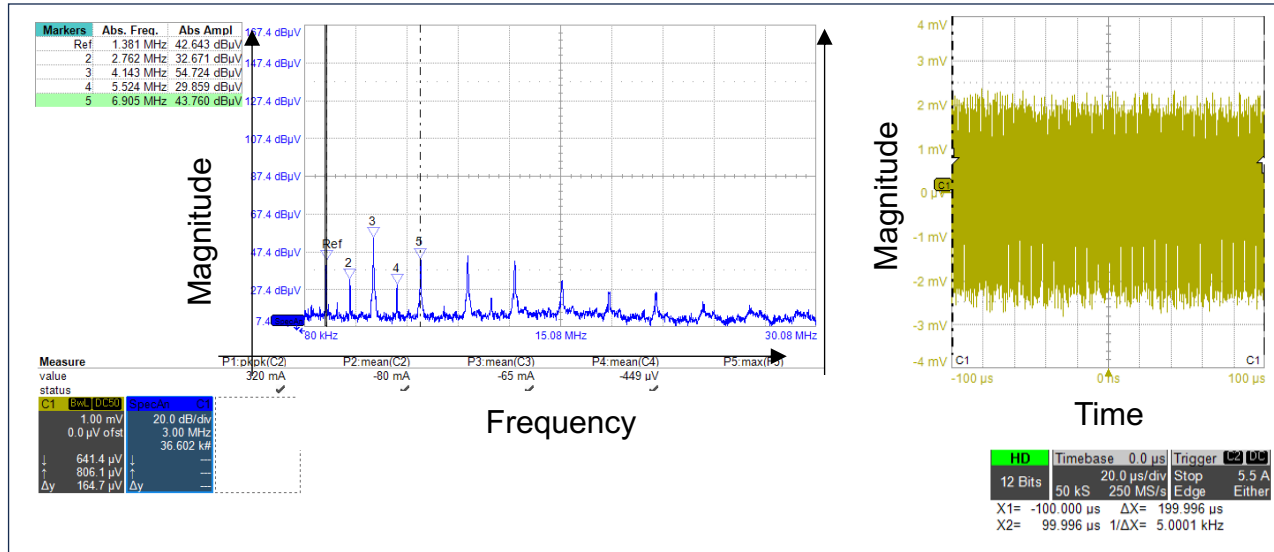
# Is the DUT Common Mode noise Load dependent?

NO,  
it isn't!





# Sensing the Common mode noise: an alternative strategy

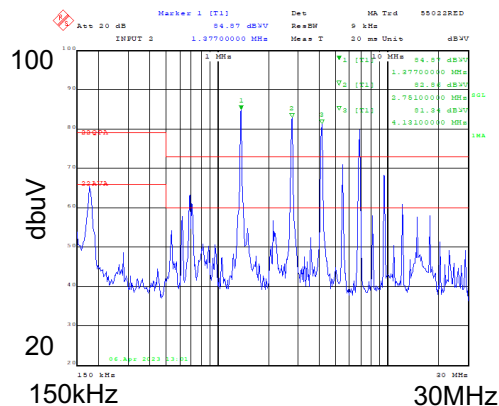


An EM “sniffer” represents a NO-invasive alternative method to extract the CM noise.

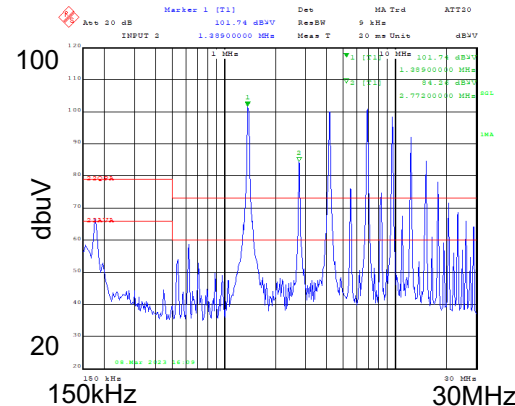
# By isolating the metallization of NBM9280 from ground plane, the noise level can be reduced.



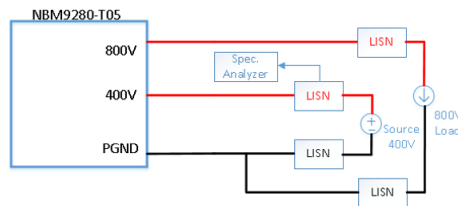
No load – metallization isolated from ground plane



No load – metallization connected to ground plane



	Metallization connected to GND [dBuV]	Metallization Isolated from GND [dBuV]
1	101.74	84.87
2	84.26	82.86
3	100	81.34
4	~76	~71
5	~100	~80
6	~75	~58

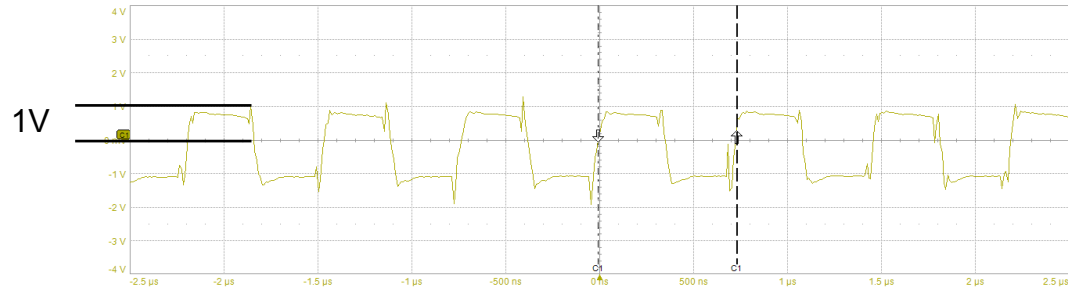


Test setup

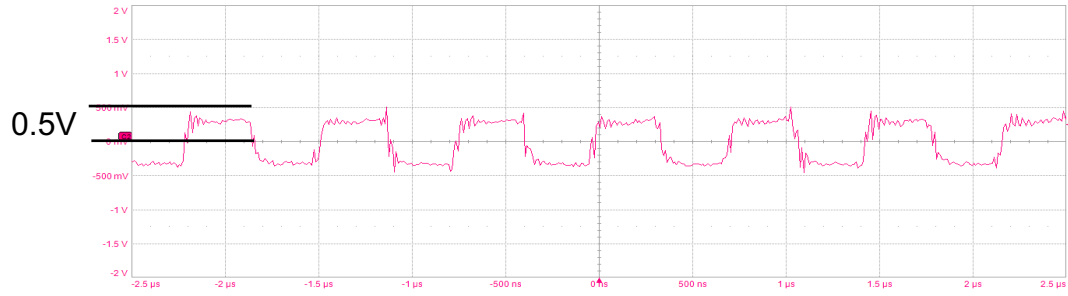
Conducted Emission  
Peak measurement  
effect of keeping the  
metallization isolated

# The bypass Capacitor: can we choose it arbitrarily?

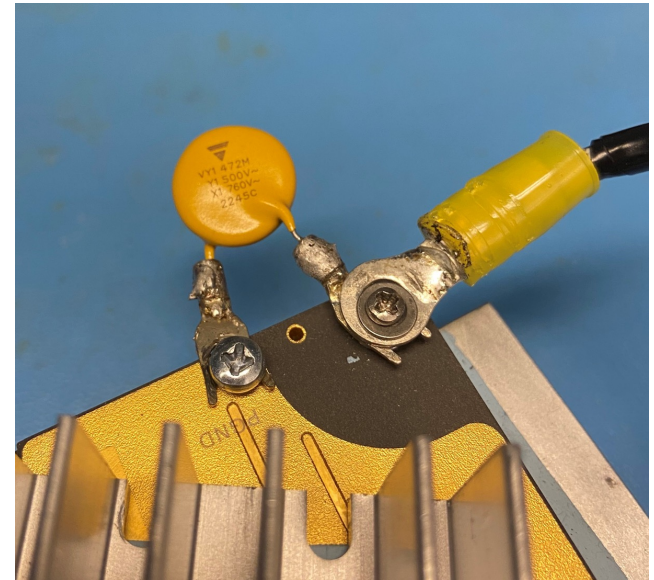
Without bypass capacitor



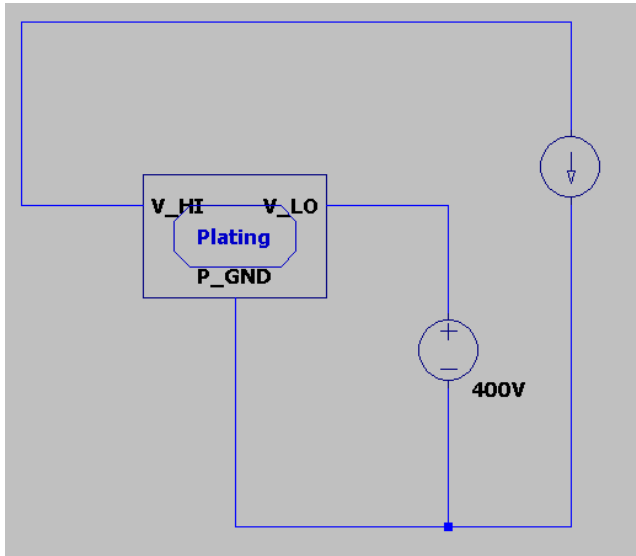
With bypass capacitor



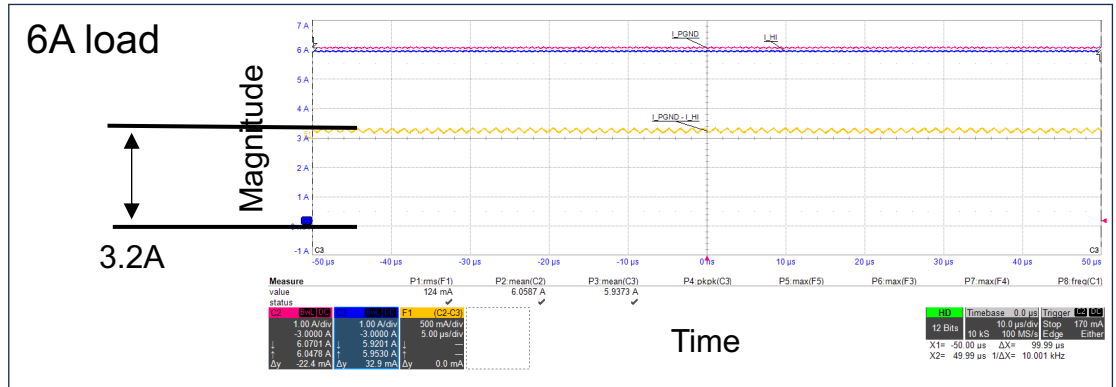
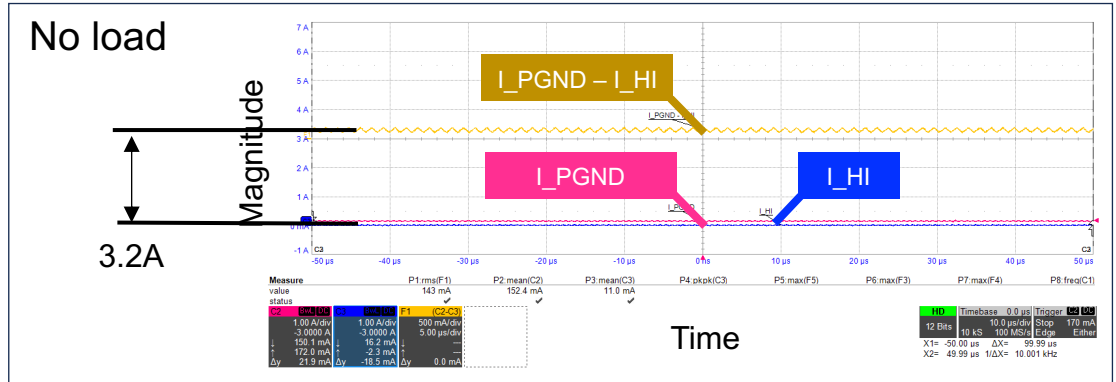
The noise level on metallization of NBM9280 with and without 4.7nF bypass Y caps



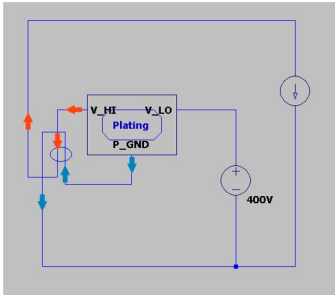
# Current Unbalanced: The current on the HI path and PGND path is not equal !!!



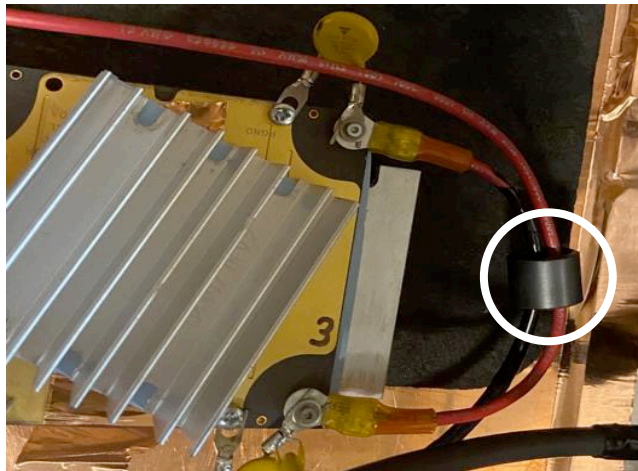
The current direction in step-up mode is shown.



# Improving the Unbalanced Current Condition



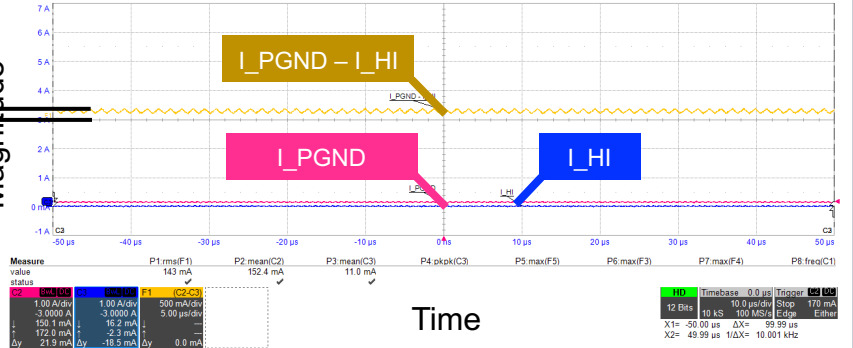
One way to smoothen the ripple on  $I_{PGND} - I_{HI}$  is to use a ferrite core on HI and PGND wire in a way the currents oppose each other.



No load

<250mA

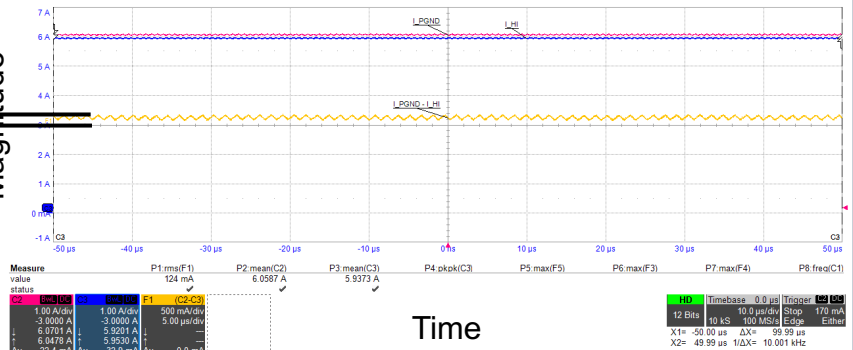
Magnitude



6A load

<250mA

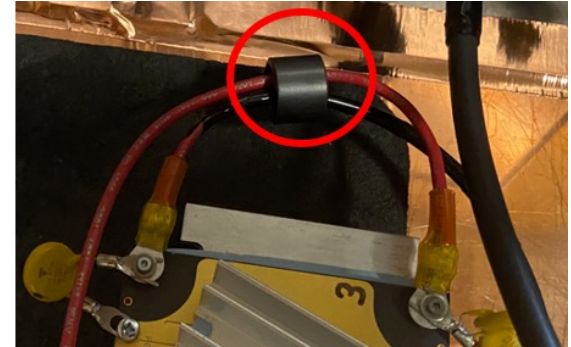
Magnitude



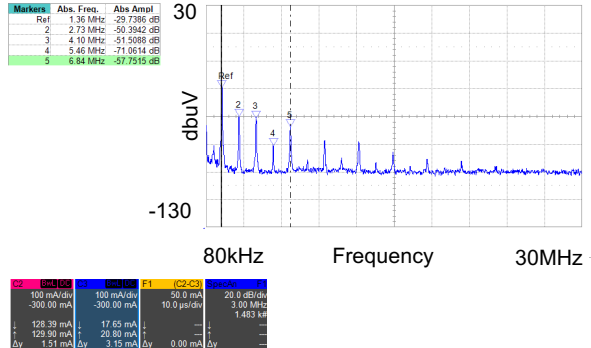
# Spectrum of IPGND – IHI

- One way to implement such a is shown as follows
- Implementing this solution on the PCB can be challenging due to the very high integration level of the part

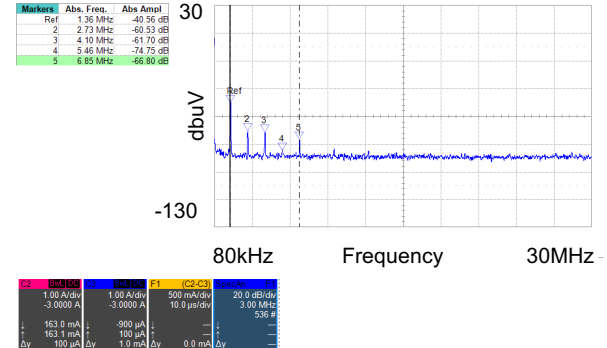
Ferrite core part #  
2643626302



No Ferrite  
on  
HI/PGND

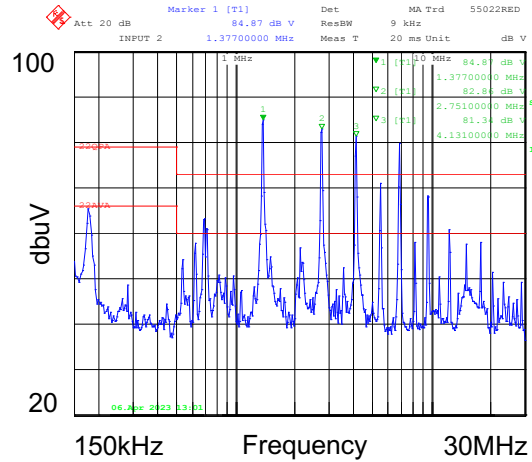


With Ferrite  
on  
HI/PGND

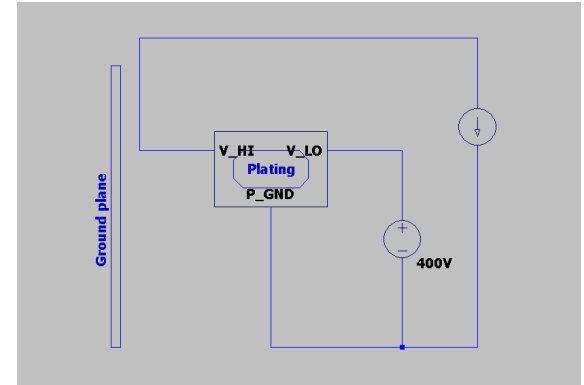
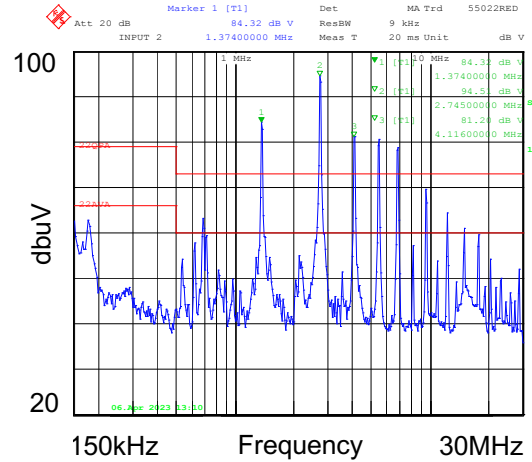


# Conducted Emission – Base Line

No load

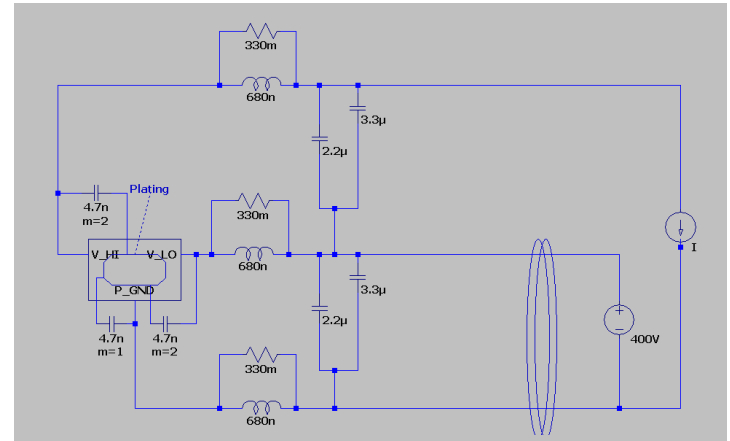
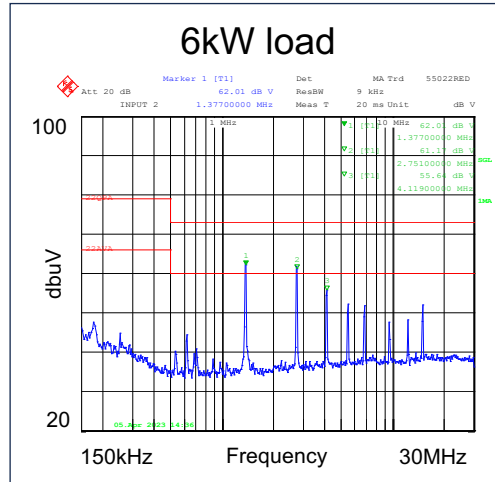
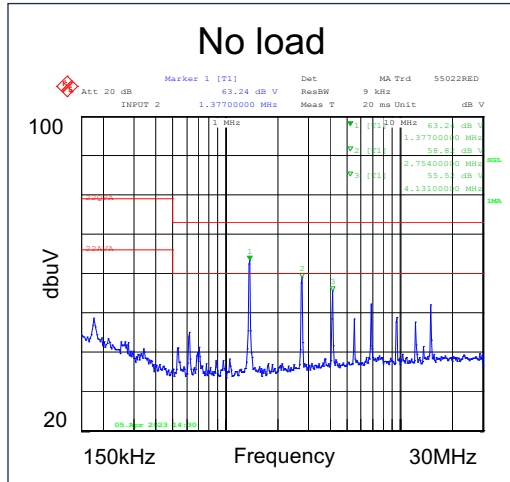


6kW load

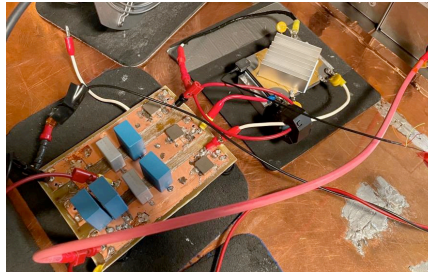


	No Load [dBuV]	6kW load [dBuV]
1	84.87	84.32
2	82.86	94.51
3	81.34	81.20
4	~71	~80
5	~80	~78
6	~58	~57

# Peak Measurement and BOM of filter #2 out of 4



	No Load [dBuV]	6kW load [dBuV]
1st	63.24	62.01
2nd	58.62	61.17
3rd	55.52	55.64
4th	~47	~52
5th	~53	~52



QTY	Part #
2	BFC233922225
2	B32924J3335K
3	MPXV1D1770LR68
5	VY1472M61Y5UC63V0
1	00431176451
3	330 mOhm resistor



# Summary of the Results

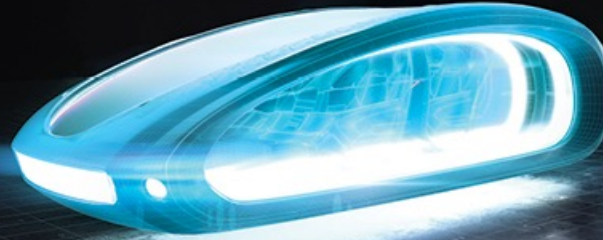
	No Filter (metallization not Isolated)	No Filter (metallization Isolated)	Filter #1	Filter #2	Filter #3	Filter #4
1 <sup>st</sup> [dBuV] @ 1.37MHz	101.74	84.87	63.24	47.9	52.37	55.6
2 <sup>nd</sup> [dBuV] @ 2.75MHz	84.26	82.86	58.62	55.25	55.75	55.6
3 <sup>rd</sup> [dBuV] @ 4.13MHz	100	81.34	55.52	41.8	40.56	46.1
4 <sup>th</sup> [dBuV] @ 5.5MHz	~76	~71	~47	~42	~46	44.95
5 <sup>th</sup> [dBuV] @ 6.88MHz	~100	~80	~53	~40	~44	~45
Rate of 2 <sup>nd</sup> increase due to loading [dBuV/kW]	~3.34	~3.34	0.41	0.67	~0	~0

# Conclusions

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- Amplitude of odd harmonics are load independent
  - However, even harmonics will increase as the result of loading.
- Keeping the metallization on NBM9280 isolated from the ground improves the EMI conducted emission result.
- The increase in the 2nd harmonic component can be mitigated by implementing PI filter.
- Satisfying CISPR 25-Class 4 & 5 (more stringent limits) still needs more attenuation on the 1st harmonics
  - One possible solution is implementing a ferrite core on HI/PGND which results in more attenuation on 1st harmonic
  - Or considering a double stage filter

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**Thank you**

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**Questions?**

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